

# **STRAIGHT STEEL GIRDER BRIDGES**

**2<sup>nd</sup> Edition, 1<sup>st</sup> Printing, November 2021**

## **REVISION LIST - 20 JANUARY 2022**

The following revisions to the first printing of the CISC publication, *Straight Steel Girder Bridges*, 2<sup>nd</sup> Edition, will be incorporated into future printings. Minor editorial revisions are not shown.

<b>Page(s)</b>	<b>Revisions</b>
1-101	<i>Replace page 1-101 with the following page. Revisions are highlighted in red.</i>

## Tensile resistance of top flange

75% of the factored tensile resistance of the top flange:

$$0.75 T_r = 0.75 \phi_s A_g F_y = 0.75 \times 0.95 (9380) 350 = 2340 \text{ kN}$$

The design force for the top flange splice is the greater of 800 and 2340 kN = 2340 kN

### 1. Tensile resistance of flange plate, ULS

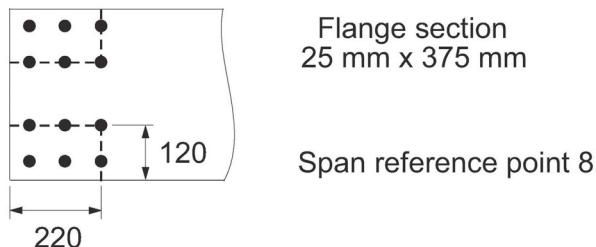
a) Fracture on the net section, Clause 10.8.2(b)

Assume a fracture plane through a transverse row of bolts

Net flange area,  $A_n = w_n t = (375 - 4 \times 29) 25 = 6480 \text{ mm}^2$

$$T_r = \phi_u A_n F_u = 0.8 \times 6480 \times 480 = 2490 \text{ kN} > 2340 \text{ kN}$$

b) Block shear, smaller flange plate, Clause 10.8.1.3.2.5



**Figure 1-28 Block shear involving combined tension + shear**

$$A_n = 2(120 - 1.5 \times 29) 25 = 3830 \text{ mm}$$

$$A_{gv} = 2(220) 25 = 11000 \text{ mm}^2$$

$$U_t = 0.9 \text{ (CISC Commentary on CSA S16:19 in Ref. 13)}$$

$$T_r = \phi_u [U_t A_n F_u + 0.6 A_{gv} F_m] = 0.75 [0.9 \times 3830 \times 480 + 0.6 \times 11000 (480 + 350) / 2] = 3300 \text{ kN} > 2340 \text{ kN}$$

### 2. Tensile resistance of splice plates, ULS

Inside splice plates: 2 x 16 mm x 160 mm

Outside splice plate: 14 mm x 375 mm

a) Yielding on the gross section, Clause 10.8.2(a)

$$A_g = 2 \times 16 \times 160 + 14 \times 375 = 10400 \text{ mm}^2$$

$$T_r = \phi_s A_g F_y = 0.95 \times 10400 \times 350 = 3460 \text{ kN} > 2340 \text{ kN}$$